

## Specification Amendments

Page 3, last paragraph (lines 26-30):

The section preferably isolates the cavity from external forces outside and adjacent the cavity. The section preferably includes a transmitting and emitting screen. The screen can be of an annular shape, or of a circular shape, or of a ~~rhombhedron~~ rhombohedron shape.

Page 11, lines 4-8:

The section 20 preferably isolates the cavity 12 from external forces outside and adjacent the cavity 12. The section 20 preferably includes a transmitting and emitting screen 24. The screen 24 can be of an annular shape, or of a circular shape, or of a ~~rhombhedron~~ rhombohedron shape.

Page 28, lines 13-26:

The numerical calculations were done with the FMT-developed special secondary emission code FMTSEC, where FMTSEC is defined as a particle-in-cell computer

simulation code capable of handling secondary emission. It is a completely self-consistent two-dimensional relativistic particle-in-cell code which treats cartesian ( $x$ - $y$ ), cylindrical ( $r$ - $z$ ), and polar ( $r$ - $\theta$ ) geometries. The field solving algorithm leapfrogs the electromagnetic fields on a staggered mesh and solves Gauss' law by diffusing away numerical errors arising from the particle-to-grid apportionment (i.e., Marder's algorithm [B. Marder, Journal of Computational Physics, 68, 48 (1987)]). The particle pusher is a Runge-Kutta second-order accurate algorithm. The charge accumulation scheme is area weighting. Graphics are done by post-processing, and dump files corresponding to values of the electric field and current density at specific points within the gun are generated.

Page 45, lines 1-12:

In this section the growth rate of the diocotron instability (an important criterion for studying the stability of hollow beam equilibrium) for the hollow beam we are considering for a microwave generator application is evaluated. The e-folding time is given by

$$\tau_e = (4 / \sqrt{4c - b^2}) (\Omega_c / \omega_p^2)$$

where  $\Omega_c = eB/m$  and the geometric factors  $c$  and  $b$  are expressed in the following form

$$b = l \left[ (1 - (r_1/r_2)^2) + \left| (r_2/r_c)^{2l} - (r_1/r_2)^{2l} \right| \right]$$

$$- (r_1/r_c)^2 \left[ 1 - (r_1/r_c)^{2l} \right] - \left[ (1 - (r_1/r_2)^{2l}) \left[ (1 - (r_2/r_c)^{2l}) \right] \right] \quad (40)$$

and have defined  $r_1, r_2, r_c$  to be the inner and outer beam radii and outer conductor radius

respectively and  $l$  is the azimuthal mode number. The worst case to consider is for the  $l=2$

mode. For the example parameters:  $n=6.25 \times 10^{11} \text{cm}^{-3}$  (100 nC/cm<sup>3</sup>),  $B=4.5$  kG,

$r_1=2.68 \text{ cm}$ ,  $r_2=3.04 \text{ cm}$  and  $r_c=3.09 \text{ cm}$ , the e-folding time is about 2 nsec. This e-

folding time allows a transport length of meters. This length is suitable for microwave generation.